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| **U.S. Radiocommunications Sector**  **Fact Sheet** | |
| **Working Party:** ITU-R WP-5B | **Document No:** USWP5B30-XX-FS |
| **Ref:** Annex 20 to Document 5B/649-E | **Date:** 11 August 2022 |
| **Document Title:** PRELIMINARY DRAFT NEW RECOMMENDATION ITU-R M.[15.4-15.7\_GHz\_ARNS] - Characteristics of and protection criteria for radars operating in the aeronautical radionavigation service in the frequency band 15.4-15.7 GHz. | |
| **Author(s)/Contributors(s):**  Don Nellis  Federal Aviation Administration  800 Independence Ave., S.W.  Washington, DC 20591  Mohammed Rahman  Federal Aviation Administration  800 Independence Ave., S.W.  Washington, DC 20591  Taylor King  ACES Corporation for DON CIO | Phone: (202) 267-9779  e-mail: Donald.Nellis@faa.gov  Phone: (202) 267-6573  e-mail: Mohammed.Rahman@faa.gov  Phone: (443) 966-0550  e-mail: Taylor.King@aces-inc.com |
| **Purpose/Objective:** The purpose of this contribution is to continue to develop a new recommendation for aeronautical radionavigation systems, including unmanned aircraft systems (UAS) Detect and Avoid (DAA) radar systems, in the 15.4-15.7 GHz band. | |
| **Abstract:** This contribution will continue the process of developing a new recommendation containing characteristics of and protection criteria for systems that operate in the 15.4-15.7 GHz aeronautical radionavigation service allocation including UAS DAA systems and will address comments received from other administrations during the previous ITU-R WP-5B meeting. Due to the stability of the technical characteristics data for the airborne and ground based DAA system as well as the technical characteristics data for the landing system, this contribution proposes to upgrade the Working Document into Preliminary Draft New Recommendation. This contribution will be an update to the new report found in Annex 20 of the Chairman’s Report of the 5 August 2022 Document 5B/649-E hybrid meeting. | |

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| **Radiocommunication Study Groups** |  |
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| **English only** |
| Annex 20 to Working Party 5B Chairman’s Report | |
| PRELIMINARY DRAFT NEW  RECOMMENDATION ITU-R M.[15.4-15.7\_GHz\_ARNS][[1]](#footnote-1)\* | |
| Characteristics of and protection criteria for radars operating in the  aeronautical radionavigation service in the frequency  band 15.4-15.7 GHz | |

(202X)

[Editor’s Note: During the July 2022 WP 5B meeting, it was agreed that further work was required to fully develop this document. This additional work needs to include a more robust description of the Detect and Avoid (DAA) radar systems similar to what is found in Section 5 of Annex 1 in Recommendation [ITU-R M.1796-2](https://www.itu.int/rec/R-REC-M.1796/en). The description should include scanning strategies, operations in and around airports, interference detection capacities, and operating conditions. The work also needs to improve the protection criteria section of this recommendation to include protection information for pulsed interferes and continuous noise-like interferes as well as the aggregate impact of interference from multiple sources of interference and multiple types of interference (see Annex 2 of Recommendation ITU-R M.1796-2). In addition, information on the relationship between the DAA radars in this Recommendation and DAA radars in other ITU-R Recommendations such as M.1796-2 would be helpful. Finally, the relationship and compatibility requirements for airborne and ground based DAA radars that are proposed for this band.]

Scope

This Recommendation specifies the characteristics and protection criteria of radars operating in the aeronautical radionavigation service (ARNS) in the frequency band 15.4-15.7 GHz. The technical and operational characteristics should be used in analysing compatibility between radars operating in the aeronautical radionavigation service and systems in other services.

Keywords

15.4-15.7 GHz, radar, characteristics, protection.

Abbreviations/Glossary

ABDAA: Airborne detect and avoid

ARNS: Aeronautical radionavigation service

ATC: Air traffic control

DAA: Detect and avoid

DV Declaration Volume

e.i.r.p: Effective isotropically radiated power

ESA: Electronically scanned array

FMCW: Frequency-modulated continuous wave

GBDAA: Ground based detect and avoid

LFM: Linear frequency modulation

OV Operational Volume

PSD: Power spectral density

RCS Radar cross-section

RR: Radio Regulation

SNR Signal-to-Noise power Ratio

UA: Unmanned aircraft

UAS: Unmanned aircraft system

Related ITU Recommendations, Reports

Recommendations

ITU-R [M.1372](https://www.itu.int/rec/R-REC-M.1372/en) Efficient use of the radio spectrum by radar stations in the radiodetermination service

ITU-R [M.1730](https://www.itu.int/rec/R-REC-M.1730/en) Characteristics of and protection criteria for the radiolocation service in the frequency band 15.4-17.3 GHz

ITU-R [S.1340](https://www.itu.int/rec/R-REC-S.1340-0-199710-I/en) Sharing between feeder links for the mobile-satellite service and the aeronautical radionavigation service in the Earth-to-space direction in the band 15.4-15.7 GHz

Report

ITU-R [M.2204](https://www.itu.int/pub/R-REP-M.2204) Characteristics and spectrum considerations for sense and avoid systems use on Unmanned Aircraft Systems (UAS)

The ITU Radiocommunication Assembly,

considering

*a)* that antenna, signal propagation, target detection, and wide necessary bandwidth of radar required to achieve their functions are optimum in certain frequency bands;

*b)* that the technical characteristics of radars operating in the aeronautical radionavigation service (ARNS) are determined by the mission of the system and vary widely even within a frequency band;

*c)* that the performance characteristics of receivers should be adequate to ensure that they do not suffer from interference due to transmitters situated at a reasonable distance and which operate in accordance with these Regulations,

recognizing

*a)* that the frequency band 15.4-15.7 GHz is allocated on a primary basis to aeronautical radionavigation, and radiolocation services, and that the fixed-satellite service (Earth-to-space) is also allocated on a primary basis in the frequency band 15.43-15.63 GHz;

*b)* that the radiolocation services operating in the frequency band 15.4-15.7 GHz shall not cause harmful interference to, or claim protection from the aeronautical radionavigation service;

*c)* that numerous features of radiodetermination radars can be expected to help suppress low-duty cycle (less than 5%) pulsed interference, especially from a few isolated sources. Techniques for suppression of low-duty cycle pulsed interference between two or more pulsed system are contained in Recommendation ITU-R M.1372 – Efficient use of the radio spectrum by radar stations in the radiodetermination service;

*d)* that the fixed-satellite service (Earth-to-space) operating in the frequency band 15.43‑15.63 GHz is limited to feeder links of non-geostationary systems in the mobile-satellite service and is subject to coordination under Radio Regulation (RR) No. **9.11A**;

*e)* that the limit of effective isotropically radiated power (e.i.r.p) of stations operating in the aeronautical radionavigation service is provided in Recommendation ITU-R S.1340;

*f)* that for stations operating in the fixed-satellite service (Earth-to-space), the minimum coordination distance required to protect the aeronautical radionavigation stations (RR No. **4.10** applies) from harmful interference from feeder-link earth stations and the maximum e.i.r.p. transmitted towards the local horizontal plane by a feeder-link earth station are provided in Recommendation ITU-R S.1340;

*g)* that for some specific systems performance requirements may be available,

[Editor’s Note: Due to the need to improve the protection criteria, two different groups of recommends are presented below. Merging of these two groups of recommends should be undertaken once the protection criteria has been updated.]

**[**

**Recommends Group A:**

recommends

1 that the technical and operational characteristics of the radars operating in the ARNS described in the Annex should be considered representative of those operating in the frequency band 15.4-15.7 GHz and used in studies of compatibility with systems in other services;

2 that, in the absence of performance requirements, the criterion of interfering signal power to radar receiver noise power level (*I*/*N)* of −6 dB, should be used as the required protection level for the aeronautical radionavigation radars, and that this represents the aggregate protection level if multiple interferers are present[[[2]](#footnote-2)];

3 that in the case of pulsed interference, the criteria should be based on a case-by-case analysis taking into account *recognizing c)* above and the undesired pulse train characteristics and, to the extent possible, the signal processing in the radar receiver,]

**Recommends Group B:**

recommends

1 that the technical and operational characteristics of the radars operating in the ARNS described in the Annex should be considered representative of those operating in the frequency band 15.4-15.7 GHz and used in studies of compatibility with systems in other services;

2 that the criterion of interfering signal power to radar receiver noise power level (*I*/*N)* of [−6 dB/−10 dB], should be used as the required protection level for the aeronautical radionavigation radars, and that this represents the aggregate protection level if multiple interferers are present.

[Editor’s note: Some administrations are of the view that the essence of deleted text and footnote in recommends 2 has been addressed in section 4, Protection criteria by referencing elements from ITU‑R M.1372 and ITU-R M.1730.]

*[Editor’s note: R*ecommends *3 and*recognizing c address similar topics, and need to be reviewed]

[Recommends Group B proposes to delete *recommends* 3 since *recognizing c)* references Recommendation ITU-R M.1372 that establishes procedure for pulsed radar interference. Furthermore, Section 4, Protection criteria of this document also addresses low-duty cycle pulsed interference radar.]

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Annex  
  
Technical and operational characteristics of radars operating in the  
aeronautical radionavigation service in the  
frequency band 15.4-15.7 GHz

# 1 Introduction

ARNS system operates on a primary basis in the frequency band 15.4-15.7 GHz. This Annex presents the technical and operational characteristics of representative ARNS radars operating in this frequency band.

Some ARNS systems are installed in unmanned aircraft (UA) or on the ground to detect non-cooperative aircraft as a surveillance system contributing to the UA detect and avoid (DAA) system. These radars are used for collision avoidance on-board UA and can be used as a part of the integration of unmanned aircraft system (UAS)[ in non-segregated airspace].

[Editor’s Note: The text in square brackets above has been proposed for deletion by some Administrations while other Administrations wish to keep the text.]

Some ARNS systems are used for landing.

# 2 Description of the Detect and Avoid (DAA) radar systems Characteristics

*[Editor’s note: the benefit from ground based detect and avoid is not justified compared to the airborne detect and avoid. Consistently with the French contribution on Handbook on DAA, it is important to address first the need for airborne systems.*

*It seems not appropriate to address in the same system “Air-to-air and Ground-to-Air aeronautical radionavigation DAA radar” which each would require totally different performance requirements. The choice of modulation as FMCW is also questionnable. What are the detailed scenarios and types of UAS that are expected to be addressed with these systems.*

*For example, maximum altitude up to 20 km is not understandable for the ground based DAA, if the intent is to complement existing surveillance systems.]*

# 2.1 Airborne detect-and-avoid (ABDAA) Radar

ABDAA radars are being developed for the purpose of enhancing flight safety by providing warnings of potential collisions or conflicts with non-cooperative aircraft2. The mission of this class of airborne radars encompasses several partially-overlapping functions referred to as collision avoidance, conflict avoidance, self-separation, safe separation, sense-and-avoid and due regard. This class of radars is of particular interest in unmanned aircraft (UA) applications where there is no onboard pilot to provide the safety-of-flight function visually.

Detect-and-avoid radars must track all potentially threatening aircraft (called ‘intruders’) in their field of regard while simultaneously searching for new threats. Since more than one intruder will frequently be in the radar’s field of regard, a multi-target tracker is required. This requires either fairly rapid track-while-scan operation, or alternatively, interleaved search and track functions in a mode called ‘search while track’ in which the track updates are scheduled as they are required. This type of operation requires beam agility beyond the capability of a mechanically scanned antenna. For this reason, airborne DAA radars typically use either electronically scanned antennas or beamforming techniques to provide the required search and track functions.

The range required for detection and tracking depends on the amount of warning time required. This in turn depends on the speed of the host platform (called the ‘ownship’), the speed of intruder aircraft, the ownship’s manoeuvring capability, the type of avoidance manoeuvre (e.g. lateral vs vertical) and delays in initiating and executing the avoidance manoeuvre. A relatively fast UA with limited manoeuvrability would require a sensor with a greater range than a slower, more manoeuvrable UA.

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2 Aircraft that are not equipped with an air traffic control radar beacon system transponder, automatic dependent surveillance-broadcast system, traffic alert and collision avoidance system or airborne collision avoidance system].

aircraft

# 2.2 Ground based detect-and-avoid (GBDAA) Radar

GBDAA is used for air traffic surveillance in support of DAA operations for unmanned aircraft. GBDAA detects and generate tracks within its Declaration Volume (DV) of airborne traffics. Unlike primary radars, DAA radars detect aircraft that flies at relatively low altitudes with smaller radar cross-sections.

As with the ABDAA, GBDAA compliments other surveillance sensors by providing detection of non-cooperative traffic (i.e., those without operating transponders or ADS-B Out capabilities). Aircraft tracks are established at sufficient range and accuracy to enable an UA flying within GBDAA Operational Volume (OV) to remain well clear of other aircraft.

FIGURE 1

Ground-based detect and avoid

Presently, in the 15.4-15.7 GHz band, there are no significant differences between the GBDAA and ABDAA systems. The requirements is simply to support the safety case, whether that’s achieved with airborne sensors, ground-based sensors, or both. However, it should be noted that the capability of ground-based vs airborne radar is different. A GBDAA radar looking up can see both in front, behind and aircraft of interest, whereas an ABDAA radar onboard the aircraft is generally pointed in the direction of flight and can only detect objects across a field of view in the direction it’s pointed. Additionally, smaller UAS are limited in the size and power of radar they can carry, whereas ground based radar has less limitation with regards to size or weight. There are also different technical challenges; for example, with GBDAA where line-of-sight over hills and buildings will need to be considered during implementation whereas with ABDAA implementation may require careful consideration of ground clutter (and returns from objects on the ground more generally) at low altitudes.

GBDAA systems use ground based sensor as the surveillance sensor and may have multiple GBDAA sensors to cover the necessary Surveillance Volume. The GBDAA can be utilized to enable transit operations, or operations at lower altitudes in area near airports as well as to enable extended operations.

# 3 Characteristics of aeronautical radionavigation detect and avoid radar

FIGURE 1

Ground-based detect and avoid

The technical parameters are provided in Table 1.

TABLE 1

Representative technical parameters of radionavigation radar

| Parameter | Units | | Radar 1 (Air) | | Radar 1 (Ground) | Radar 2 (Air) | Radar 2 (Ground) | Radar 3 (Air) | Radar 3 (Ground) |
| --- | --- | --- | --- | --- | --- | --- | --- | --- | --- |
| Platform |  | | Aircraft | | Ground (on and off airports) | Aircraft | Ground (on and off airports) | Airborne | Ground |
| Platform height | km | | Up to 12 | | 0 | Up to 12 | 0 | Up to 12 | 0 |
| Spectral usage |  | | Air-to-air aeronautical radionavigation DAA radar | | Ground-to-Air aeronautical radionavigation DAA radar | Air-to-air aeronautical radionavigation DAA radar | Ground-to-Air aeronautical radionavigation DAA radar | Air-to-air aeronautical radionavigation DAA radar | Ground-to-Air aeronautical radionavigation DAA radar |
| Radar type |  | | FMCW | | FMCW | FMCW | FMCW | Pulse-Doppler | Pulse-Doppler |
| Range class |  | | Short range | | Short range | Short range | Short range | Medium range | Medium range |
| Operating range | km | | 0.8 (small UAS) 2.0 (small General Aviation aircraft) | | TBD | 1.8 (small UAS) 4.5 (small General Aviation aircraft) | TBD | 9 | TBD |
| Maximum number of drones within the same operating area |  | | 10 to 20 | | 32 | 10 to 20 | 32 | 3 | 12 |
| Ground speed | km/h | | 200 | | 0 | 200 | 0 | < 700 | 0 |
| Frequency tuning range | GHz | | 15.4-15.7 (Note 1) | | 15.4-15.7 (Note 1) | 15.4-15.7 (Note 1) | 15.4-15.7 (Note 1) | 15.4-15.7 (Note 2) | 15.4-15.7 (Note 2) |
| Channel selection method between radars |  | | (Note 1) | | (Note 1) | (Note 1) | (Note 1) | SW selectable (Note 3) | SW selectable (Note 3) |
| Emission type |  | | QXN | | QXN | QXN | QXN | FXN | FXN |
| Modulation |  | | FMCW | | FMCW | FMCW | FMCW | LFM |  |
| Pulse width (1 meter range resolution) | μs | | 220 | | 220 | 197 | 197 | 0.25 to 20  (Note 4) | 0.25 to 20  (Note 4) |
| Pulse rise and fall times | μs | | 5/5 | | 5/5 | 0.5/0.5 | 0.5/0.5 | < 0.1 | < 0.1 |
| RF emission bandwidth   −3 dB  −20 dB  −40 dB | MHz | | 176  184  201 | | 176  184  201 | 152  164  269 | 152  164  269 | (Band 1-MHz)  25  80  155 | (Band 1-MHz)  25  80  155 |
| Pulse repetition frequency | ps | | 4000 | | 4000 | 4000 | 4000 | 1-200 | 1-200 |
| Average transmitter power (conducted) | W | | 2 | | 2 | 10 | 10 | 30 | 30 |
| Out-of-band emission characteristics | dBc | | < 50 | | < 50 | < 40 | < 40 | <-75 (through 3rd harmonic) | <-75 (through 3rd harmonic) |
| Spurious emission characteristics (conducted) | dBc | | -72 | | -72 | -87 | -87 | -60 | -60 |
| Receiver IF bandwidth  −3 dB  −20 dB  −60 dB | MHz | | 15  32  58 | | 15  32  58 | 15  32  58 | 15  32  58 | <200  <300  <400 | <200  <300  <400 |
| Sensitivity | dBm | | -147 | | -147 | -141 | -141 | -121 | -121 |
| Receiver noise figure | dB | | 1.5 | | 1.5 | 1.5 | 1.5 | 4 | 4 |
| Calculated Rx noise power | dBW | | -130.7 | | -130.7 | -130.7 | -130.7 | -133  (Note 5) | -133  (Note 5) |
| Saturation level | dBW/m2 | | -35 | | -35 | -30 | -30 | -40 | -40 |
| Effective Incident RX Thermal Noise power | dBW/m2 | | -176.6 | | -176.6 | -176.6 | -176.6 | -107.5 | -107.5 |
| Antenna type |  | | Bi-Static Phased Array | | Bi-Static Phased Array | Bi-Static Phased Array | Bi-Static Phased Array | ESA (Note 6) | ESA (Note 6) |
| Antenna placement |  | | Aircraft (manned or unmanned) | | Tower (<20 m) | Aircraft (manned  or unmanned) | Tower (<20 m) | Aircraft (manned or unmanned) | Tower (<20 m) (internally sealed package) |
| RX Element gain | dBi | | 2 | | 2 | 2 | 2 | 27 | 27 |
| Antenna gain | dBi | | 12 | | 12 | 15 | 15 | 27 | 27 |
| First TX antenna side lobe | dBi | | -3 at 50° | | -3 at 50° | -1 at 52° | -1 at 52° | <-20 | <-20 |
| Horizontal beamwidth | degrees | | 40 | | 40 | 32 | 32 | 4 | 4 |
| Vertical beamwidth | degrees | | 40 | | 40 | 28 | 28 | 2 | 2 |
| Polarization |  | | Vertical | | Vertical | Horizontal | Horizontal | Horizontal | Horizontal |
| Horizontal Antenna scan | degrees | | ±60 | | ±60 | ±60 | ±60 | ± 65 | ± 65 |
| Vertical Antenna scan | degrees | | ±20 | | ±20 | ±60 | ±60 | -40, +50 | -40, +50 |
|  | |  | | Notes:  1 Radar is pre-programmed at the factory to any centre frequency inside this band. The set range resolution directly affects BW. Therefore, the range resolution will be a factor when programming the centre frequency, to ensure that the spectral power is within the 15.4 to 15.7 GHz band. For radars set with larger RR (i.e. smaller BW’s), multiple radars can be programmed and operated inside the 15.4 to 15.7 GHz band, allowing for coverage of larger areas.  2 Utilized bandwidth - Inclusive of frequency-channel guard-bands.  3 Channel selection is purely SW-defined and can be on-the-fly dynamic. Some settings may allow radar to self-configure based on detected spectrum-conflict.  4 Waveform is software-defined on a CPI-by-CPI basis, and optimized for targets, and spectral environments.  5 Compressed bandwidth before processing gain.  6 High T/R ESA RF beamforming on both transmit and receive. | | | | |  |

# 4 Characteristics of aeronautical radionavigation landing system

This system is an electronic landing aid that provides flight path data to an approaching aircraft as the aircraft flies into range of the landing system. There are two separate surface transmitters, one for azimuth and one for elevation, as well as a receiver installed on the aircraft. The system utilizes a one-way transmission where the angular information is displayed on a cross-point indicator allowing the aircraft to align itself with the runway.

The technical parameters are provided in Table 2.

TABLE 2

Technical parameters of landing system

| Parameter | Units | Transmitter | Receiver |
| --- | --- | --- | --- |
| Platform |  | Land/Ship | Aircraft |
| Platform height | km | Land: 0.01 Ship: 0.015-0.024 | Maximum: 2 |
| Ground speed | km/h | Land: 0 Ship: < 50 | < 350 |
| Number of aircraft per landing system |  | 1 | 1 |
| Frequency tuning range | GHz | 15.4-15.7 | 15.4-15.7 |
| Emission type |  | Pulse | Not applicable |
| Pulse width | μs | 0.3 | Not applicable |
| Pulse rise and fall times | ns | Rise Time: 25-50;  Fall Time: 25-200 | Not applicable |
| RF emission bandwidth at   −3 dB  −20 dB  −40 dB | MHz | 4.8  18.5  65 | Not applicable |
| Pulse repetition frequency | pps | 15000 | Not applicable |
| Out-of-band emission characteristics | dBc | <43 | Not applicable |
| Spurious emission characteristics | dBc | 65 | Not applicable |
| Average transmitter power | W | Peak: 2500;  Average: 7 | Not applicable |
| Receiver IF bandwidth at  −3 dB  −20 dB  −60 dB | MHz | Not applicable | 12  17  24 |
| Sensitivity | dBm | Not applicable | −72 |
| Receiver noise figure | dB | Not applicable | 11.5 |
| Calculated Rx noise power | dBW | Not applicable | −121.7 |
| Image rejection | dB | Not applicable | 60 |
| Spurious rejection | dB | Not applicable | 50 |
| Antenna type |  | Parabolic Reflector | Horn |
| Antenna placement |  | Ground/Surface | Bottom of aircraft |
| Antenna gain | dBi | Horizontal: 32;  Vertical: 26 | 6 |
| First antenna side lobe | dBi | At least 17 dB below peak | At least 17 dB below peak |
| Horizontal beamwidth | degrees | Horizontal: 40;  Vertical: 2 | 70 |
| Vertical beamwidth | degrees | Horizontal: 1.3; Vertical: 6 | 36 |
| Polarization |  | Vertical | Vertical |
| Antenna scan | degrees | Sector Scan | Fixed |

# 5 Protection criteria

**5.1 Continuous noise-like interference**

Radars are affected in fundamentally different ways by unwanted signals of different forms, and an especially sharp difference prevails between the effects of continuous noise-like energy and those of pulses. Continuous-wave interference of a noise-like type inflicts a desensitizing effect on radiodetermination radars, and that effect is predictably related to its intensity. The desensitizing effect on radars from other services of a continuous-wave or noise-like type modulation is predictably related to its intensity. In any azimuth sectors in which such interference arrives, its power spectral density (PSD) can, to within a reasonable approximation, simply be added to the PSD of the radar receiver thermal noise. If PSD of radar‑receiver noise in the absence of interference is denoted by *N*0 and that of noise-like interference by *I*0, the resultant effective noise PSD becomes simply *I*0 + *N*0.

Given that, the radar protection criteria traditionally established within ITU-R are based on the penalties incurred to maintain the target-return signal-to-noise ratio in the presence of the interference, requiring that the target-return power be raised in proportion to the increase of noise power from *N*0 to *I*0 + *N*0. That can only be done by accepting shorter maximum ranges on given targets, sacrificing observation of small targets, or modifying the radar to give it a higher transmitter power or power-aperture product.

These penalties vary depending on the radar’s function and the nature of its targets. For most radars, an increase in the effective noise level of about 1 dB would inflict the maximum tolerable degradation on performance. In the case of a discrete target having a given average or median Radar cross-section (RCS), that increase would reduce the detection range by about 6% regardless of any RCS fluctuation characteristics that target might have. This effect results from the fact that the achievable free-space range is proportional to the 4th root of the resultant signal-to-noise power ratio (SNR), from the most familiar form of the radar range equation. A 1 dB increase of effective noise power is a factor of 1.26 in power, so it would, if uncompensated, require the free-space range from a given discrete target to be reduced by a factor of 1/(1.261/4), or 1/1.06; i.e. a range capability reduction of about 6%. In the range equation, the SNR is also directly proportional to transmitter power, to power-aperture product (for a surveillance radar), and to target radar cross section. Alternatively, therefore, the 1 dB increase of effective noise power could be compensated by forgoing detection of targets except those having an average radar cross section 1.26 times as large as the minimum-size target that could be detected in the interference-free regime or by increasing the radar transmitter power or its power-aperture product by 26%. Any of these alternatives is at the limit of acceptability in most radar missions, and the system modifications would be costly, impractical, or impossible, especially in mobile radars. For discrete targets, those performance penalties hold for any given probability of detection and false-alarm rate and any target fluctuation characteristics.

**5.1.1 Aggregation of interference contributions**

The 1 dB increase referred to throughout the above discussions corresponds to an (I + N)/N ratio of 1.26, or an I/N of about −6 dB. This represents the tolerable aggregate effect of all interferers. It applies for reception via the radar’s main beam as well as for simultaneous reception via side lobes. The tolerable I/N for an individual noise-like interferer therefore depends on the number of interferers and their geometry and should be assessed in the analysis of a given scenario. This is a consequence of the fact that almost all the radars in this band serve event-driven missions, observe non-cooperative targets, and do not have the benefit of redundancy, including the re-transmission of packets that is becoming used more and more in communications technologies. Basically, sensing, including radar, is a fundamentally different use of the RF spectrum than is communications, and the same interference-protection rules are not appropriate for both.

**5.2 Pulsed interference** The effect of pulsed interference is more difficult to quantify and is strongly dependent on receiver/processor design and mode of operation. In particular, the differential processing gains for valid-target return, which is synchronously pulsed, and interference pulses, which are usually asynchronous, often have important effects on the impact of given levels of pulsed interference. Several different forms of performance degradation can be inflicted by such desensitization. Assessing it will be an objective for analyses of interactions between specific radar types. Assessing it will be an objective for analysis of interactions between specific pulsed radar types.

In general, numerous features of radiodetermination radars can be expected to help suppress low-duty cycle pulsed interference, especially from a few isolated sources. Techniques for suppression of low-duty cycle pulsed interference are contained in Recommendation ITU-R M.1372 – *Efficient use of the radio spectrum by radar stations in the radiodetermination service*. When multiple interferers are present, the recommended *I/N* protection criteria remains unchanged. The total interference level actually arriving at the radar receiver depends on the number of interferers, their spatial distribution and their signal structure and needs to be assessed in the course of an aggregation analysis of a given scenario. If interference were received from several azimuth directions, an aggregation analysis has to cumulate simultaneous contributions from all these directions, being received via the radar antenna’s main beam and/or side-lobes, in order to assess compatibility.

[

*– For typical radars an increase of about 1 dB would constitute significant degradation, equivalent to a detection-range reduction of about 6%. Such an increase corresponds to an I/N ratio of 1.26, or an I/N ratio of about −6 dB.*

*– For the radionavigation service considering the safety-of-life function, an increase of about 0.5 dB would constitute significant degradation. Such an increase corresponds to an (I/N) ratio of −10 dB.]*

[Editor’s Note: The text in square brackets above has been proposed for deletion by some Administrations while other Administrations wish to keep the text. Work to improve the protection criteria section in this recommendation needs to address the relevance of this text.]

These protection criteria represent the aggregate effects of multiple interferers, when present; the allowable *I*/*N* ratio for an individual interferer depends on the number of interferers and their geometry and needs to be assessed in the course of analysis of a given scenario. The aggregation factor can be very substantial in the case of certain communication systems in which a great number of stations can be deployed.

1. \* This Recommendation should be brought to the attention of the International Civil Aviation Organization (ICAO). [↑](#footnote-ref-1)
2. [The criterion of protection does not include aeronautical safety margin.] [↑](#footnote-ref-2)